# **MCP651/1S/2/3/4/5/9**

## **50 MHz, 200 µV Op Amps with mCal**

#### **Features:**

- Gain-Bandwidth Product: 50 MHz
- Slew Rate: 30 V/µs
- Low Input Offset: ±200 µV (maximum)
- Low Input Bias Current: 6 pA (typical)
- Noise:  $7.5$  nV/ $\sqrt{Hz}$ , at 1 MHz
- Ease-of-Use:
	- Unity-Gain Stable
	- Rail-to-Rail Output
	- Input Range incl. Negative Rail
	- No Phase Reversal
- Supply Voltage Range: +2.5V to +5.5V
- High Output Current: ±100 mA
- Supply Current: 6.0 mA/Ch (typical)
- Low-Power Mode: 5 µA/Ch
- Small Packages: SOT23-5, DFN
- Extended Temperature Range: -40°C to +125°C

## **Typical Applications:**

- Driving A/D Converters
- Fast Low-side Current Sensing
- Power Amplifier Control Loops
- Optical Detector Amplifier
- Barcode Scanners
- Multi-Pole Active Filter
- Consumer Audio

## **Design Aids:**

- SPICE Macro Models
- FilterLab<sup>®</sup> Software
- Microchip Advanced Part Selector (MAPS)
- Analog Demonstration and Evaluation Boards - MCP651EV-VOS
- Application Notes

## **Description:**

The Microchip Technology Inc. MCP651/1S/2/3/4/5/9 family of high bandwidth and high slew rate operational amplifiers features low offset. At power-up, these op amps are self-calibrated using mCal. Some package options also provide a Calibration/Chip Select pin (CAL/CS) that supports a Low-Power mode of operation, with offset calibration at the time normal operation is re-started. These amplifiers are optimized for high speed, low noise and distortion, single-supply operation with rail-to-rail output and an input that includes the negative rail.

This family is offered in single (MCP651 and MCP651S), single with CAL/CS pin (MCP653), dual (MCP652), dual with CAL/CS pins (MCP655), quad (MCP654) and quad with CAL/CS pins (MCP659). All devices are fully specified from -40°C to +125°C.

## **Typical Application Circuit**





## <span id="page-0-0"></span> **High Gain-Bandwidth Op Amp Portfolio**

## **MCP651/1S/2/3/4/5/9**



## **Package Types**

## **1.0 ELECTRICAL CHARACTERISTICS**

## <span id="page-2-3"></span>**1.1 Absolute Maximum Ratings †**



**† Notice:** Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at those or any other conditions above those indicated in the operational listings of this specification is not implied. Exposure to maximum rating conditions for extended periods may affect device reliability.

**††** See **[Section 4.2.2 "Input Voltage and Current Limits"](#page-22-0)**.

## **1.2 Specifications**

## **TABLE 1-1: DC ELECTRICAL SPECIFICATIONS**

**Electrical Characteristics:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ ,  $V_L = V_{\text{DD}}/2$ ,  $R_L = 1$  k $\Omega$  to  $V_L$  and CAL/CS =  $V_{SS}$  (refer to [Figure 1-2](#page-6-0)).



<span id="page-2-1"></span><span id="page-2-0"></span>**Note 1:** Describes the offset (under the specified conditions) right after power-up, or just after the CAL/CS pin is toggled. Thus, 1/f noise effects (an apparent wander in  $V_{OS}$ ; see [Figure 2-35\)](#page-14-0) are not included.

<span id="page-2-2"></span>**2:** See [Figure 2-6](#page-7-0) and [Figure 2-7](#page-8-0) for temperature effects.

**3:** The I<sub>SC</sub> specifications are for design guidance only; they are not tested.

## **TABLE 1-1: DC ELECTRICAL SPECIFICATIONS (CONTINUED)**

**Electrical Characteristics:** Unless otherwise indicated, T<sub>A</sub> = +25°C, V<sub>DD</sub> = +2.5V to +5.5V, V<sub>SS</sub> = GND, V<sub>CM</sub> = V<sub>DD</sub>/3,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ ,  $V_{\text{L}} = V_{\text{DD}}/2$ ,  $R_{\text{L}} = 1$  k $\Omega$  to  $V_{\text{L}}$  and CAL/CS =  $V_{\text{SS}}$  (refer to Figure 1-2).



Note 1: Describes the offset (under the specified conditions) right after power-up, or just after the CAL/CS pin is toggled. Thus, 1/f noise effects (an apparent wander in  $V_{OS}$ ; see Figure 2-35) are not included.

**2:** See Figure 2-6 and Figure 2-7 for temperature effects.

**3:** The I<sub>SC</sub> specifications are for design guidance only; they are not tested.

## **TABLE 1-2: AC ELECTRICAL SPECIFICATIONS**

**Electrical Characteristics:** Unless otherwise indicated,  $T_A = 25^\circ C$ ,  $V_{DD} = +2.5V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $\sqrt{V_{\text{OUT}}} \approx V_{\text{DD}}/2$ ,  $V_L = V_{\text{DD}}/2$ ,  $R_L = 1$  kΩ to  $V_L$ ,  $C_L = 20$  pF and CAL/CS =  $V_{SS}$  (refer to [Figure 1-2\)](#page-6-0).





## <span id="page-4-3"></span>**TABLE 1-3: DIGITAL ELECTRICAL SPECIFICATIONS**

<span id="page-4-0"></span>**Note 1:** The MCP652 single, MCP653 single, MCP655 dual and MCP659 quad have their CAL/CS inputs internally pulled down to  $V_{SS}$  (0V).

**2:** This time ensures that the internal logic recognizes the edge. However, for the rising edge case, if CAL/CS is raised before the calibration is complete, the calibration will be aborted and the part will return to Low-Power mode.

<span id="page-4-1"></span>**3:** For the MCP655 dual, there is an additional constraint. CALA/CSA and CALB/CSB can be toggled simultaneously (within a time much smaller than  $t_{CSU}$ ) to make both op amps perform the same function simultaneously. If they are toggled independently, then CALA/CSA (CALB/CSB) cannot be allowed to toggle while op amp B (op amp A) is in Calibration mode; allow more than the maximum  $t_{CON}$  time (4 ms) before the other side is toggled.

<span id="page-4-2"></span>**4:** For the MCP659 quad, there is an additional constraint. CALAD/CSAD and CALBC/CSBC can be toggled simultaneously (within a time much smaller than  $t_{CSU}$ ) to make all four op amps perform the same function simultaneously, and the maximum  $t_{\text{CON}}$  time is approximately doubled (8 ms). If they are toggled independently, then CALAD/CSAD (CALBC/CSBC) cannot be allowed to toggle while op amps B and C (op amps A and D) are in Calibration mode; allow more than the maximum  $t_{CON}$  time (8 ms) before the other side is toggled.

<span id="page-5-3"></span>



<span id="page-5-2"></span><span id="page-5-1"></span>**Note 1:** Operation must not cause T<sub>J</sub> to exceed Maximum Junction Temperature specification (150°C).<br>2: Measured on a standard JC51-7, four-layer printed circuit board with ground plane and vias.

**2:** Measured on a standard JC51-7, four-layer printed circuit board with ground plane and vias.

## **1.3 Timing Diagram**



**Note**: For the MCP655 dual and the MCP659 quad, there is an additional constraint on toggling the two CAL/CS pins close together; see the  $T_{CON}$  specification in Table 1-3.

<span id="page-5-0"></span>*FIGURE 1-1: Timing Diagram.*

## **1.4 Test Circuits**

The circuit used for most DC and AC tests is shown in [Figure 1-2.](#page-6-0) This circuit can independently set  $V_{CM}$  and  $\rm V_{\rm OUT}$ ; see [Equation 1-1.](#page-6-1) Note that  $\rm V_{CM}$  is not the circuit's Common mode voltage ((V<sub>P</sub> + V<sub>M</sub>)/2), and that  $V_{OST}$  includes  $V_{OS}$  plus the effects (on the input offset error,  $V_{OST}$ ) of temperature, CMRR, PSRR and  $A_{OL}$ .

#### <span id="page-6-1"></span>**EQUATION 1-1:**

 $G_{DM} = R_F/R_G$  $V_{CM} = (V_P + V_{DD}/2)/2$  $V_{OUT} = (V_{DD}/2) + (V_P - V_M) + V_{OST}(1 + G_{DM})$ Where: *G<sub>DM</sub>* = Differential Mode Gain (V/V) *VCM* = Op Amp's Common Mode Input Voltage (V)  $V_{OST}$  = Op Amp's Total Input Offset Voltage (mV)  $V_{OST} = V_{IN-} - V_{IN+}$ 



<span id="page-6-0"></span>*FIGURE 1-2: AC and DC Test Circuit for Most Specifications.*

## **2.0 TYPICAL PERFORMANCE CURVES**

**Note:** The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

## **2.1 DC Signal Inputs**



*FIGURE 2-1: Input Offset Voltage.*



*FIGURE 2-2: Input Offset Voltage Drift.*



*FIGURE 2-3: Input Offset Voltage Repeatability (repeated calibration).*



*FIGURE 2-4: Input Offset Voltage vs. Power Supply Voltage.*



*Output Voltage.*

*FIGURE 2-5: Input Offset Voltage vs.* 



<span id="page-7-0"></span>

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .



<span id="page-8-0"></span>*FIGURE 2-7: High-Input Common Mode Voltage Headroom vs. Ambient Temperature.*



*FIGURE 2-8: Input Offset Voltage vs. Common Mode Voltage with V<sub>DD</sub>* = 2.5V.



*FIGURE 2-9: Input Offset Voltage vs. Common Mode Voltage with V<sub>DD</sub> = 5.5V.* 



*FIGURE 2-10: CMRR and PSRR vs. Ambient Temperature.*



*FIGURE 2-11: DC Open-Loop Gain vs. Ambient Temperature.*



*FIGURE 2-12: Input Bias and Offset Currents vs. Ambient Temperature with*   $V_{DD} = +5.5V$ .

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .



*FIGURE 2-13: Input Bias and Offset Currents vs. Common Mode Input Voltage with*   $T_A = +85^{\circ}C$ .



*FIGURE 2-14: Input Bias and Offset Currents vs. Common Mode Input Voltage with*   $T_A$  = +125 °C.



<span id="page-9-0"></span>*FIGURE 2-15: Input Bias Current vs. Input Voltage (below V<sub>SS</sub>).* 

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**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

#### **14**  $V_{DD} = 5.5V$  $\mathbb{I}$  $\pm$ **Ratio of Output Headroom to**  $V_{OL} - V_{SS}$ **Output Current (mV/mA) 12** -I<sub>OUT</sub> **10 8 6**  $V_{DD} - V_{OP}$ **I**<sub>OUT</sub> **4**  $V_{DD} = 2.5V$ **2 0 1 10 100 Output Current Magnitude (mA)**

## **2.2 Other DC Voltages and Currents**

<span id="page-10-0"></span>



<span id="page-10-1"></span>*FIGURE 2-17: Output Voltage Headroom vs. Ambient Temperature.*



*FIGURE 2-18: Output Short-Circuit Current vs. Power Supply Voltage.*



*FIGURE 2-19: Supply Current vs. Power Supply Voltage.*



*FIGURE 2-20: Supply Current vs. Common Mode Input Voltage.*



*FIGURE 2-21: Power-On Reset Voltages vs. Ambient Temperature.*

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L$  =  $V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .



*FIGURE 2-22: Normalized Internal Calibration Voltage.*



*Temperature.*

## **MCP651/1S/2/3/4/5/9**

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

## **2.3 Frequency Response**



*Frequency.*











*FIGURE 2-26: Gain-Bandwidth Product and Phase Margin vs. Ambient Temperature.*



*FIGURE 2-27: Gain-Bandwidth Product and Phase Margin vs. Common Mode Input Voltage.*



*FIGURE 2-28: Gain-Bandwidth Product and Phase Margin vs. Output Voltage.*



*FIGURE 2-29: Closed-Loop Output Impedance vs. Frequency.*

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L$  =  $V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .



<span id="page-13-0"></span>*FIGURE 2-30: Gain Peaking vs. Normalized Capacitive Load.*



*FIGURE 2-31: Channel-to-Channel Separation vs. Frequency.*

**Note:** Unless otherwise indicated,  $T_A$  = +25°C,  $V_{DD}$  = +2.5V to 5.5V,  $V_{SS}$  = GND,  $V_{CM}$  =  $V_{DD}/3$ ,  $V_{OUT}$  =  $V_{DD}/2$ ,  $V_L$  =  $V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

#### **2.4 Input Noise and Distortion**



*FIGURE 2-32: Input Noise Voltage Density vs. Frequency.*



*FIGURE 2-33: Input Noise Voltage Density vs. Input Common Mode Voltage with f = 100 Hz.*



*FIGURE 2-34: Input Noise Voltage Density vs. Input Common Mode Voltage with f = 1 MHz.*



<span id="page-14-0"></span>*FIGURE 2-35: Input Noise plus Offset vs. Time with 0.1 Hz Filter.*



*FIGURE 2-36: THD+N vs. Frequency.*

## **MCP651/1S/2/3/4/5/9**

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

## **2.5 Time Response**



<span id="page-15-1"></span>*FIGURE 2-37: Non-inverting Small Signal Step Response.*



<span id="page-15-2"></span>*FIGURE 2-38: Non-inverting Large Signal Step Response.*



*Response.*

<span id="page-15-3"></span>*FIGURE 2-39: Inverting Small Signal Step* 



<span id="page-15-4"></span>*FIGURE 2-40: Inverting Large Signal Step Response.*



<span id="page-15-0"></span>*FIGURE 2-41: The MCP651/1S/2/3/4/5/9 family shows no input phase reversal with overdrive.*



*Temperature.*

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} =$  GND,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 1$  k $\Omega$  to  $V_L$ ,  $C_L = 20$  pF, and CAL/CS =  $V_{SS}$ .



*FIGURE 2-43: Maximum Output Voltage Swing vs. Frequency.*

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}$ C,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ , R<sub>L</sub> = 1 k $\Omega$  to  $V_L$ , C<sub>L</sub> = 20 pF, and CAL/CS =  $V_{SS}$ .

## **2.6 Calibration and Chip Select Response**



*FIGURE 2-44: CAL/CS Current vs. Power Supply Voltage.*



*FIGURE 2-45: CAL/CS Voltage, Output Voltage and Supply Current (for Side A) vs. Time with*  $V_{DD} = 2.5V$ .



*FIGURE 2-46: CAL/CS Voltage, Output Voltage and Supply Current (for Side A) vs. Time with*  $V_{DD} = 5.5V$ .



*FIGURE 2-47: CAL/CS Hysteresis vs. Ambient Temperature.*



*FIGURE 2-48: CAL/CS Turn-On Time vs. Ambient Temperature.*



*FIGURE 2-49: CAL/CS's Pull-Down Resistor (R<sub>PD</sub>) vs. Ambient Temperature.* 

**Note:** Unless otherwise indicated,  $T_A = +25^{\circ}C$ ,  $V_{DD} = +2.5V$  to 5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/3$ ,  $V_{OUT} = V_{DD}/2$ ,  $V_L = V_{DD}/2$ ,  $R_L = 1$  k $\Omega$  to  $V_L$ ,  $C_L = 20$  pF, and CAL/CS =  $V_{SS}$ .



*FIGURE 2-50: Quiescent Current in Shutdown vs. Power Supply Voltage.*



*Output Voltage.*

## **3.0 PIN DESCRIPTIONS**

Descriptions of the pins are listed in [Table 3-1](#page-19-0).

## <span id="page-19-0"></span>**TABLE 3-1: PIN FUNCTION TABLE**



## **3.1 Analog Outputs**

The analog output pins  $(V<sub>OUT</sub>)$  are low-impedance voltage sources.

## **3.2 Analog Inputs**

The non-inverting and inverting inputs  $(V_{IN}+, V_{IN}-, ...)$ are high-impedance CMOS inputs with low bias currents.

## **3.3 Power Supply Pins**

The positive power supply  $(V_{DD})$  is 2.5V to 5.5V higher than the negative power supply  $(V_{SS})$ . For normal operation, the other pins are between  $V_{SS}$  and  $V_{DD}$ .

Typically, these parts are used in a single (positive) supply configuration. In this case,  $V_{SS}$  is connected to ground and  $V_{DD}$  is connected to the supply.  $V_{DD}$  will need bypass capacitors.

## **3.4 Calibration Common Mode Voltage Input**

A low-impedance voltage placed at this input  $(V_{CAI})$ will set the op amps' Common mode input voltage during calibration. If this pin is left open, the Common mode input voltage during calibration is approximately  $V<sub>DD</sub>/3$ . The internal resistor divider is disconnected from the supplies whenever the part is not in calibration.

## **3.5 Calibrate/Chip Select Digital Input**

This input (CAL/CS, …) is a CMOS, Schmitt-Triggered input that affects the Calibration and Low-Power modes of operation. When this pin goes high, the part is placed into a Low-Power mode and the output is High Z. When this pin goes low, a calibration sequence is started (which corrects  $V_{OS}$ ). At the end of the calibration sequence, the output becomes low-impedance and the part resumes normal operation.

An internal POR triggers a calibration event when the part is powered on, or when the supply voltage drops too low. Thus, the MCP652 parts are calibrated, even though they do not have a CAL/CS pin.

## **3.6 Exposed Thermal Pad (EP)**

There is an internal connection between the Exposed Thermal Pad (EP) and the  $V_{SS}$  pin; they must be connected to the same potential on the Printed Circuit Board (PCB).

This pad can be connected to a PCB ground plane to provide a larger heat sink. This improves the package thermal resistance  $(\theta_{JA})$ .

## **4.0 APPLICATIONS**

The MCP651/1S/2/3/4/5/9 family of self-zeroed op amps is manufactured using Microchip's state-of-theart CMOS process. It is designed for low-cost, lowpower and high-precision applications. Its low supply voltage, low quiescent current and wide bandwidth makes the MCP651/1S/2/3/4/5/9 ideal for batterypowered applications.

## **4.1 Calibration and Chip Select**

These op amps include circuitry for dynamic calibration of the offset voltage  $(V_{OS})$ .

## 4.1.1 mCal CALIBRATION CIRCUITRY

The internal mCal circuitry, when activated, starts a delay timer (to wait for the op amp to settle to its new bias point), then calibrates the input offset voltage  $(V_{OS})$ . The mCal circuitry is triggered at power-up (and after some power brown-out events) by the internal POR, and by the memory's Parity Detector. The powerup time, when the mCal circuitry triggers the calibration sequence, is 200 ms (typical).

## $4.1.2$  CAL/CS PIN

The CAL/CS pin gives the user a means to externally demand a Low-Power mode of operation, then to calibrate  $V_{OS}$ . Using the CAL/CS pin makes it possible to correct  $V_{OS}$  as it drifts over time (1/f noise and aging; see [Figure 2-35\)](#page-14-0) and across temperature.

The CAL/CS pin performs two functions: it places the op amp(s) in a Low-Power mode when it is held high, and starts a calibration event (correction of  $V_{OS}$ ) after a rising edge.

While in the Low-Power mode, the quiescent current is quite small ( $I_{SS}$  = -3 µA, typical). The output is also in a High Z state.

During the calibration event, the quiescent current is near, but smaller than, the specified quiescent current (6 mA, typical). The output continues in the High Z state, and the inputs are disconnected from the external circuit, to prevent internal signals from affecting circuit operation. The op amp inputs are internally connected to a Common mode voltage buffer and feedback resistors. The offset is corrected (using a digital state machine, logic and memory), and the calibration constants are stored in memory.

Once the calibration event is completed, the amplifier is reconnected to the external circuitry. The turn-on time, when calibration is started with the CAL/ $\overline{\text{CS}}$  pin, is 3 ms (typical).

There is an internal 5 M $\Omega$  pull-down resistor tied to the CAL/CS pin. If the CAL/CS pin is left floating, the amplifier operates normally.

For the MCP655 dual and the MCP659 quad, there is an additional constraint on toggling the two CAL/CS pins close together; see the  $t_{\text{CON}}$  specification in [Table 1-3.](#page-4-3) If the two pins are toggled simultaneously, or if they are toggled separately with an adequate delay between them (greater than  $t_{\text{CON}}$ ), then the CAL/CS inputs are accepted as valid. If one of the two pins toggles while the other pin's calibration routine is in progress, then an invalid input occurs and the result is unpredictable.

## 4.1.3 INTERNAL POR

This part includes an internal Power-On Reset (POR) to protect the internal calibration memory cells. The POR monitors the power supply voltage  $(V_{DD})$ . When the POR detects a low  $V_{DD}$  event, it places the part into the Low-Power mode of operation. When the POR detects a normal  $V_{DD}$  event, it starts a delay counter, then triggers an calibration event. The additional delay gives a total POR turn-on time of 200 ms (typical); this is also the power-up time (since the POR is triggered at power-up).

## 4.1.4 PARITY DETECTOR

A parity error detector monitors the memory contents for any corruption. In the rare event that a parity error is detected (e.g., corruption from an alpha particle), a POR event is automatically triggered. This will cause the input offset voltage to be re-corrected, and the op amp will not return to normal operation for a period of time (the POR turn-on time,  $t_{PON}$ ).

## 4.1.5 CALIBRATION INPUT PIN

A  $V_{\text{CAI}}$  pin is available in some options (e.g., the single MCP651) for those applications that need the calibration to occur at an internally driven Common mode voltage other than  $V_{DD}/3$ .

[Figure 4-1](#page-21-0) shows the reference circuit that internally sets the op amp's Common mode reference voltage  $(V<sub>CM</sub>INT)$  during calibration (the resistors are disconnected from the supplies at other times). The  $5 k\Omega$  resistor provides over-current protection for the buffer.



*Input Circuitry.*

<span id="page-21-0"></span>*FIGURE 4-1: Common-Mode Reference's* 

When the  $V_{CAL}$  pin is left open, the internal resistor divider generates a  $V_{CM\_INT}$  of approximately  $V_{DD}/3$ , which is near the center of the input Common mode voltage range. It is recommended that an external capacitor from  $V_{CAL}$  to ground be added to improve noise immunity.

When the  $V_{CAL}$  pin is driven by an external voltage source, which is within its specified range, the op amp will have its input offset voltage calibrated at that Common mode input voltage. Make sure that  $V_{CAI}$  is within its specified range.

It is possible to use an external resistor voltage divider to modify  $V_{CM~INT}$ ; see [Figure 4-2.](#page-22-1) The internal circuitry at the V<sub>CAL</sub> pin looks like 100 k $\Omega$  tied to V<sub>DD</sub>/3. The parallel equivalent of  $R_1$  and  $R_2$  should be much smaller than 100 k $\Omega$  to minimize differences in matching and temperature drift between the internal and external resistors. Again, make sure that  $V_{CAI}$  is within its specified range.



<span id="page-22-1"></span>**FIGURE 4-2:** Setting V<sub>CM</sub> with External *Resistors.*

For instance, a design goal to set  $V_{CM~INT} = 0.1V$  when  $V_{DD}$  = 2.5V could be met with:  $R_1$  = 24.3 k $\Omega$ ,  $R_2$  = 1.00 k $\Omega$  and C<sub>1</sub> = 100 nF. This will keep V<sub>CAL</sub> within its range for any  $V_{DD}$ , and should be close enough to 0V for ground-based applications.

#### **4.2 Input**

#### 4.2.1 PHASE REVERSAL

The input devices are designed to not exhibit phase inversion when the input pins exceed the supply voltages. [Figure 2-41](#page-15-0) shows an input voltage exceeding both supplies with no phase inversion.

#### <span id="page-22-0"></span>4.2.2 INPUT VOLTAGE AND CURRENT LIMITS

The ESD protection on the inputs can be depicted as shown in [Figure 4-3.](#page-22-2) This structure was chosen to protect the input transistors, and to minimize input bias current  $(I_B)$ . The input ESD diodes clamp the inputs when they try to go more than one diode drop below  $V_{SS}$ . They also clamp any voltages that go too far above  $V_{DD}$ ; their breakdown voltage is high enough to allow normal operation, and low enough to bypass quick ESD events within the specified limits.



<span id="page-22-2"></span>*FIGURE 4-3: Simplified Analog Input ESD Structures.*

In order to prevent damage and/or improper operation of these amplifiers, the circuit must limit the currents (and voltages) at the input pins (see **[Section 1.1](#page-2-3) ["Absolute Maximum Ratings †"](#page-2-3)**). [Figure 4-4](#page-22-3) shows the recommended approach to protecting these inputs. The internal ESD diodes prevent the input pins  $(V_{IN}+$ and  $V_{\text{IN}}$ ) from going too far below ground, and the resistors  $R_1$  and  $R_2$  limit the possible current drawn out of the input pins. Diodes  $D_1$  and  $D_2$  prevent the input pins ( $V_{1N}$ + and  $V_{1N}$ –) from going too far above  $V_{DD}$ , and dump any currents onto  $V_{DD}$ . When implemented as shown, resistors  $R_1$  and  $R_2$  also limit the current through  $D_1$  and  $D_2$ .



<span id="page-22-3"></span>*FIGURE 4-4: Protecting the Analog Inputs.*

It is also possible to connect the diodes to the left of the resistor  $R_1$  and  $R_2$ . In this case, the currents through the diodes  $D_1$  and  $D_2$  need to be limited by some other mechanism. The resistors then serve as in-rush current limiters; the DC current into the input pins  $(V_{1N} +$  and  $V_{\text{IN}}$ ) should be very small.

A significant amount of current can flow out of the inputs (through the ESD diodes) when the Common mode voltage  $(V_{CM})$  is below ground  $(V_{SS})$ ; see [Figure 2-15.](#page-9-0) Applications that are high-impedance may need to limit the usable voltage range.

#### 4.2.3 NORMAL OPERATION

The input stage of the MCP651/1S/2/3/4/5/9 op amps uses a differential PMOS input stage. It operates at low Common mode input voltage ( $V_{CM}$ ), with  $V_{CM}$  up to  $V_{DD}$  – 1.3V and down to  $V_{SS}$  – 0.3V. The input offset voltage ( $V_{OS}$ ) is measured at  $V_{CM} = V_{SS} - 0.3V$  and  $V<sub>DD</sub> - 1.3V$  to ensure proper operation. See [Figure 2-6](#page-7-0) and [Figure 2-7](#page-8-0) for temperature effects.

When operating at very low non-inverting gains, the output voltage is limited at the top by the  $V_{CM}$  range  $(< V_{DD} - 1.3V)$ ; see [Figure 4-5.](#page-23-0)



<span id="page-23-0"></span>*FIGURE 4-5: Unity-Gain Voltage Limitations for Linear Operation.*

## **4.3 Rail-to-Rail Output**

#### 4.3.0.1 Maximum Output Voltage

The Maximum Output Voltage (see [Figure 2-16](#page-10-0) and [Figure 2-17\)](#page-10-1) describes the output range for a given load. For instance, the output voltage swings to within 15 mV of the negative rail with a 1 k $\Omega$  load tied to  $V<sub>DD</sub>/2$ .

#### 4.3.0.2 Output Current

[Figure 4-6](#page-23-1) shows the possible combinations of output voltage ( $V_{\text{OUT}}$ ) and output current ( $I_{\text{OUT}}$ ).  $I_{\text{OUT}}$  is positive when it flows out of the op amp into the external circuit.



<span id="page-23-1"></span>*FIGURE 4-6: Output Current.*

#### 4.3.0.3 Power Dissipation

Since the output short circuit current  $(I_{SC})$  is specified at ±100 mA (typical), these op amps are capable of both delivering and dissipating significant power. Two common loads, and their impact on the op amp's power dissipation, will be discussed.

[Figure 4-7](#page-24-0) shows a resistive load  $(R<sub>1</sub>)$  with a DC output voltage ( $V_{\text{OUT}}$ ).  $V_L$  is R<sub>L</sub>'s ground point,  $V_{SS}$  is usually ground (0V) and  $I_{\text{OUT}}$  is the output current. The input currents are assumed to be negligible.



<span id="page-24-0"></span>*FIGURE 4-7: Diagram for Resistive Load Power Calculations.*

The DC currents are:

#### **EQUATION 4-1:**

$$
I_{OUT} = \frac{V_{OUT} - V_L}{R_L}
$$
  
\n
$$
I_{DD} \approx I_Q + max(0, I_{OUT})
$$
  
\n
$$
I_{SS} \approx -I_Q + min(0, I_{OUT})
$$

Where:

 $I_{\Omega}$  = Quiescent supply current for one op amp (mA/amplifier)  $V_{OUT}$  = A DC value (V)

The DC op amp power is:

#### **EQUATION 4-2:**

$$
P_{OA}\,=\,I_{DD}(V_{DD}-V_{OUT})+I_{SS}(V_{SS}-V_{OUT})
$$

The maximum op amp power, for resistive loads at DC, occurs when  $V_{OUT}$  is halfway between  $V_{DD}$  and  $V_L$  or halfway between  $V_{SS}$  and  $V_L$ :

#### **EQUATION 4-3:**

$$
max(P_{OA}) = I_{DD}(V_{DD} - V_{SS}) + \frac{max^{2}(V_{DD} - V_{L}, V_{L} - V_{SS})}{4R_{L}}
$$

[Figure 4-7](#page-24-0) shows a capacitive load  $(C_L)$ , which is driven by a sine wave with DC offset. The capacitive load causes the op amp to output higher currents at higher frequencies. Because the output rectifies  $I_{\text{OUT}}$ , the op amp's dissipated power increases (even though the capacitor does not dissipate power).



*FIGURE 4-8: Diagram for Capacitive Load Power Calculations.*

The output voltage is assumed to be:

#### **EQUATION 4-4:**

$$
V_{OUT} = V_{DC} + V_{AC} \sin(\omega t)
$$
 Where:

$$
V_{DC} = DC offset (V)
$$

- $V_{AC}$  = Peak output swing ( $V_{PK}$ )
- $\omega$  = Radian frequency ( $2\pi$  f) (rad/s)

The op amp's currents are:

#### **EQUATION 4-5:**

$$
I_{OUT} = C_L \cdot \frac{dV_{OUT}}{dt} = V_{AC} \omega C_L \cos(\omega t)
$$
  
\n
$$
I_{DD} \approx I_Q + \max(0, I_{OUT})
$$
  
\n
$$
I_{SS} \approx -I_Q + \min(0, I_{OUT})
$$
  
\nWhere:  
\n
$$
I_Q = \text{Quiescent supply current for one}
$$
  
\nop amp (mA/amplifier)

The op amp's instantaneous power, average power and peak power are:

**EQUATION 4-6:**

$$
P_{OA} = I_{DD}(V_{DD} - V_{OUT}) + I_{SS}(V_{SS} - V_{OUT})
$$
  
\n
$$
ave(P_{OA}) = (V_{DD} - V_{SS})(I_Q + \frac{4V_{AC}fC_L}{\pi})
$$
  
\n
$$
max(P_{OA}) = (V_{DD} - V_{SS})(I_Q + 2V_{AC}fC_L)
$$

The power dissipated in a package depends on the powers dissipated by each op amp in that package:

#### **EQUATION 4-7:**

Where:

 $P_{PKG} = \sum P_{OA}$  $k = 1$  $=$   $\sum$ 

n = Number of op amps in package (1 or 2)

*n*

The maximum ambient to junction temperature rise  $(\Delta T_{JA})$  and junction temperature  $(T_J)$  can be calculated using the maximum expected package power ( $P_{PKG}$ ), ambient temperature  $(T_A)$  and the package thermal resistance  $(\theta_{JA})$  found in [Table 1-4](#page-5-3):

#### **EQUATION 4-8:**

$$
\Delta T_{JA} = P_{PKG} \theta_{JA}
$$
  

$$
T_J = T_A + \Delta T_{JA}
$$

The worst-case power de-rating for the op amps in a particular package can be easily calculated:

#### **EQUATION 4-9:**

$$
P_{PKG} \le \frac{T_{Jmax} - T_A}{\theta_{JA}}
$$

Where:

*TJmax* = Absolute maximum junction temperature (°C)  $T_A$  = Ambient temperature (°C)

Several techniques are available to reduce  $\Delta T_{JA}$  for a given package:

- Reduce  $\theta_{\mathsf{JA}}$ 
	- Use another package
	- Improve the PCB layout (ground plane, etc.)
	- Add heat sinks and air flow
- Reduce  $max(P_{PKG})$ 
	- Increase  $R_1$
	- Decrease  $C_1$
	- Limit  $I_{\text{OUT}}$  using  $R_{\text{ISO}}$  (see [Figure 4-9\)](#page-25-0)
	- Decrease V<sub>DD</sub>

## **4.4 Improving Stability**

## <span id="page-25-2"></span>4.4.1 CAPACITIVE LOADS

Driving large capacitive loads can cause stability problems for voltage feedback op amps. As the load capacitance increases, the feedback loop's phase margin decreases and the closed-loop bandwidth is reduced. This produces gain peaking in the frequency response, with overshoot and ringing in the step response. See [Figure 2-30](#page-13-0). A unity-gain buffer  $(G = +1)$  is the most sensitive to capacitive loads, though all gains show the same general behavior.

When driving large capacitive loads with these op amps (e.g.,  $> 20$  pF when  $G = +1$ ), a small series resistor at the output ( $R_{\rm ISO}$  in [Figure 4-9](#page-25-0)) improves the feedback loop's phase margin (stability) by making the output load resistive at higher frequencies. The bandwidth will be generally lower than the bandwidth with no capacitive load.



<span id="page-25-0"></span>*FIGURE 4-9: Output Resistor, RISO Stabilizes Large Capacitive Loads.*

[Figure 4-10](#page-25-1) gives recommended  $R_{ISO}$  values for different capacitive loads and gains. The x-axis is the normalized load capacitance  $(C_L/G_N)$ , where  $G_N$  is the circuit's noise gain. For non-inverting gains,  $G_N$  and the Signal Gain are equal. For inverting gains,  $G_N$  is 1+|Signal Gain| (e.g., -1 V/V gives  $G_N$  = +2 V/V).



<span id="page-25-1"></span>*FIGURE 4-10: Recommended RISO Values for Capacitive Loads.*

After selecting  $R_{\text{ISO}}$  for your circuit, double check the resulting frequency response peaking and step response overshoot. Modify  $R_{\text{ISO}}$ 's value until the response is reasonable. Bench evaluation and simulations with the MCP651/1S/2/3/4/5/9 SPICE macro model are helpful.

## 4.4.2 GAIN PEAKING

[Figure 4-11](#page-26-0) shows an op amp circuit that represents non-inverting amplifiers ( $V_M$  is a DC voltage and  $V_P$  is the input) or inverting amplifiers ( $V_P$  is a DC voltage and  $V_M$  is the input). The capacitances  $C_N$  and  $C_G$ represent the total capacitance at the input pins; they include the op amp's Common mode input capacitance  $(C<sub>CM</sub>)$ , board parasitic capacitance and any capacitor placed in parallel.



<span id="page-26-0"></span>*FIGURE 4-11: Amplifier with Parasitic Capacitance.*

 $C_G$  acts in parallel with  $R_G$  (except for a gain of +1 V/V), which causes an increase in gain at high frequencies.  $C_G$  also reduces the phase margin of the feedback loop, which becomes less stable. This effect can be reduced by either reducing  $C_G$  or  $R_F$ .

 $C_N$  and  $R_N$  form a low-pass filter that affects the signal at  $V_P$ . This filter has a single real pole at  $1/(2\pi R_N C_N)$ .

The largest value of  $R_F$  that should be used depends on noise gain (see G<sub>N</sub> in **[Section 4.4.1 "Capacitive](#page-25-2) Loads**") and  $C_G$ . [Figure 4-12](#page-26-1) shows the maximum recommended  $R_F$  for several  $C_G$  values.



<span id="page-26-1"></span>*FIGURE 4-12: Maximum Recommended RF vs. Gain.*

[Figure 2-37](#page-15-1) and [Figure 2-38](#page-15-2) show the small signal and large signal step responses at  $G = +1$  V/V. The unitygain buffer usually has  $R_F = 0\Omega$  and  $R_G$  open.

[Figure 2-39](#page-15-3) and [Figure 2-40](#page-15-4) show the small signal and large signal step responses at G = -1 V/V. Since the noise gain is 2 V/V and  $C_G \approx 10$  pF, the resistors were chosen to be  $R_F = R_G = 499\Omega$  and  $R_N = 249\Omega$ .

It is also possible to add a capacitor  $(C_F)$  in parallel with  $R_F$  to compensate for the de-stabilizing effect of  $C_G$ . This makes it possible to use larger values of  $R_F$ . The conditions for stability are summarized in [Equation 4-](#page-26-2) [10.](#page-26-2)

#### <span id="page-26-2"></span>**EQUATION 4-10:**

 $f_F \leq f_{GBWP}$  *(2G<sub>N2</sub>)*,  $G_{N1} < G_{N2}$ We need:  $G_{NI} = I + R_F/R_G$  $G_{N2} = I + C_G/C_F$  $f_F = 1/(2 \pi R_F C_F)$  $f_Z = f_F(G_{N1}/G_{N2})$ Given:  $f_F \leq f_{GBWP} \leq (4G_{N1}), \quad G_{N1} > G_{N2}$ 

## **4.5 Power Supply**

With this family of operational amplifiers, the Power Supply pin  $(V_{DD}$  for single supply) should have a local bypass capacitor (i.e.,  $0.01 \mu F$  to  $0.1 \mu F$ ) within 2 mm for good high-frequency performance. Surface mount, multilayer ceramic capacitors, or their equivalent, should be used.

These op amps require a bulk capacitor (i.e., 2.2 µF or larger) within 50 mm to provide large, slow currents. Tantalum capacitors, or their equivalent, may be a good choice. This bulk capacitor can be shared with other nearby analog parts as long as crosstalk through the supplies does not prove to be a problem.

## **4.6 High-Speed PCB Layout**

These op amps are fast enough that a little extra care in the PCB (Printed Circuit Board) layout can make a significant difference in performance. Good PCB layout techniques will help achieve the performance shown in the specifications and Typical Performance Curves; it will also help minimize EMC (Electro-Magnetic Compatibility) issues.

Use a solid ground plane. Connect the bypass local capacitor(s) to this plane with minimal length traces to cut down inductive and capacitive crosstalk.

Separate digital from analog, low-speed from highspeed, and low-power from high-power. This will reduce interference.

Keep sensitive traces short and straight. Separate them from interfering components and traces. This is especially important for high-frequency (low rise time) signals.

Sometimes, it helps to place guard traces next to victim traces. They should be on both sides of the victim trace, and as close as possible. Connect guard traces to ground plane at both ends, and in the middle for long traces.

Use coax cables, or low inductance wiring, to route signal and power to and from the PCB. Mutual and self inductance of power wires is often a cause of crosstalk and unusual behavior.

## **4.7 Typical Applications**

#### 4.7.1 POWER DRIVER WITH HIGH GAIN

[Figure 4-13](#page-27-0) shows a power driver with high gain  $(1 + R<sub>2</sub>/R<sub>1</sub>)$ . The MCP651/1S/2/3/4/5/9 op amp's shortcircuit current makes it possible to drive significant loads. The calibrated input offset voltage supports accurate response at high gains.  $R_3$  should be small, and equal to  $R_1||R_2$ , in order to minimize the bias current induced offset.



<span id="page-27-0"></span>

## 4.7.2 OPTICAL DETECTOR AMPLIFIER

[Figure 4-14](#page-27-1) shows a transimpedance amplifier, using the MCP651 op amp, in a photo detector circuit. The photo detector is a capacitive current source. The op amp's input Common mode capacitance (5 pF, typical) acts in parallel with  $C_D$ . R<sub>F</sub> provides enough gain to produce 10 mV at  $V_{\text{OUT}}$ . C<sub>F</sub> stabilizes the gain and limits the transimpedance bandwidth to about 1.1 MHz.  $R<sub>F</sub>$ 's parasitic capacitance (e.g., 0.2 pF for a 0805 SMD) acts in parallel with  $C_F$ .



<span id="page-27-1"></span>*FIGURE 4-14: Transimpedance Amplifier for an Optical Detector.*

#### 4.7.3 H-BRIDGE DRIVER

[Figure 4-15](#page-27-2) shows the MCP652 dual op amp used as a H-bridge driver. The load could be a speaker or a DC motor.



<span id="page-27-2"></span>

This circuit automatically makes the noise gains  $(G_N)$ equal, when the gains are set properly, so that the frequency responses match well (in magnitude and in phase). [Equation 4-11](#page-27-3) shows how to calculate  $R<sub>GT</sub>$  and  $R<sub>GB</sub>$  so that both op amps have the same DC gains;  $G<sub>DM</sub>$  needs to be selected first.

## <span id="page-27-3"></span>**EQUATION 4-11:**

$$
G_{DM} = \frac{V_{OT} - V_{OB}}{V_{IN} - V_{DD}/2} \ge 2 \text{ V/V}
$$

$$
R_{GT} = \frac{R_F}{(G_{DM}/2) - 1}
$$

$$
R_{GB} = \frac{R_F}{G_{DM}/2}
$$

[Equation 4-12](#page-27-4) gives the resulting Common mode and Differential mode output voltages.

#### <span id="page-27-4"></span>**EQUATION 4-12:**

$$
\frac{V_{OT} + V_{OB}}{2} = \frac{V_{DD}}{2}
$$

$$
V_{OT} - V_{OB} = G_{DM} \left(V_{IN} - \frac{V_{DD}}{2}\right)
$$

## **6.0 PACKAGING INFORMATION**

## **6.1 Package Marking Information**

5-Lead SOT-23 (2x3) **(MCP651S)** Example:



6-Lead SOT-23 (2x3) **(MCP653)** Example:



8-Lead TDFN(2x3) **(MCP651)** Example:



8-Lead DFN (3x3) **(MCP652)** Example:

















## **6.2 Package Marking Information**

8-Lead SOIC (150 mil) **(MCP651, MCP652)**



10-Lead DFN (3x3) **(MCP655)** Example:



10-Lead MSOP **(MCP655)** Example:



YWWNNN

XXXXXXX





## 5-Lead Plastic Small Outline Transistor (OT) [SOT-23]











#### Notes:

1. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.127 mm per side.

2. Dimensioning and tolerancing per ASME Y14.5M.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing C04-091B

5-Lead Plastic Small Outline Transistor (OT) [SOT-23]





Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2091A

## **6-Lead Plastic Small Outline Transistor (CHY) [SOT-23]**





#### **Notes:**

- 1. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.127 mm per side.
- 2. Dimensioning and tolerancing per ASME Y14.5M.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing C04-028B

## **6-Lead Plastic Small Outline Transistor (CHY) [SOT-23]**





Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2028A



Microchip Technology Drawing No. C04-062C Sheet 1 of 2





Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.

2. Package may have one or more exposed tie bars at ends.

3. Package is saw singulated

4. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances. REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-062C Sheet 2 of 2



## RECOMMENDED LAND PATTERN



#### Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2062B

8-Lead Plastic Small Outline (SN) - Narrow, 3.90 mm Body [SOIC]



Microchip Technology Drawing No. C04-057C Sheet 1 of 2

8-Lead Plastic Small Outline (SN) - Narrow, 3.90 mm Body [SOIC]





#### Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.

2. § Significant Characteristic

- 3. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.15mm per side.
- 4. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-057C Sheet 2 of 2





RECOMMENDED LAND PATTERN



Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2057A



#### **BOTTOM VIEW**

Microchip Technology Drawing No. C04-129C Sheet 1 of 2





#### Notes:

- 1. Pin 1 visual index feature may vary, but must be located within the hatched area.
- 2. Package may have one or more exposed tie bars at ends.
- 3. Package is saw singulated
- 4. Dimensioning and tolerancing per ASME Y14.5M
	- BSC: Basic Dimension. Theoretically exact value shown without tolerances. REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-129C Sheet 2 of 2





Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2129A





Microchip Technology Drawing No. C04-063C Sheet 1 of 2





Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.<br>2. Package may have one or more exposed tie bars at ends.

3. Package is saw singulated.

4. Dimensioning and tolerancing per ASME Y14.5M.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-063C Sheet 2 of 2



## RECOMMENDED LAND PATTERN



Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2063B

10-Lead Plastic Micro Small Outline Package (UN) [MSOP]



Microchip Technology Drawing C04-021C Sheet 1 of 2

10-Lead Plastic Micro Small Outline Package (UN) [MSOP]





Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.

2. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.15mm per side.<br>3. Dimensioning and tolerancing per ASME Y14.5M.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing C04-021C Sheet 2 of 2

**10-Lead Plastic Micro Small Outline Package (UN) [MSOP]**



## RECOMMENDED LAND PATTERN



Notes

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2021A



14-Lead Plastic Small Outline (SL) - Narrow, 3.90 mm Body [SOIC]



14-Lead Plastic Small Outline (SL) - Narrow, 3.90 mm Body [SOIC]









#### Notes:

- 1. Pin 1 visual index feature may vary, but must be located within the hatched area.
- 2 § Significant Characteristic
- 3. Dimension D does not include mold flash, protrusions or gate burrs, which shall not exceed 0.15 mm per end. Dimension E1 does not include interlead flash or protrusion, which shall not exceed 0.25 mm per side.
- 4. Dimensioning and tolerancing per ASME Y14.5M BSC: Basic Dimension. Theoretically exact value shown without tolerances. REF: Reference Dimension, usually without tolerance, for information purposes only.
- 5 Datums A & B to be determined at Datum H.

Microchip Technology Drawing No. C04-065C Sheet 2 of 2

14-Lead Plastic Small Outline (SL) - Narrow, 3.90 mm Body [SOIC]



## RECOMMENDED LAND PATTERN



Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2065A

14-Lead Plastic Thin Shrink Small Outline (ST) - 4.4 mm Body [TSSOP]





Microchip Technology Drawing C04-087C Sheet 1 of 2

## 14-Lead Plastic Thin Shrink Small Outline (ST) - 4.4 mm Body [TSSOP]





Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.

2. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.15mm per side.

3. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances. REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-087C Sheet 2 of 2

14-Lead Plastic Thin Shrink Small Outline (ST) - 4.4 mm Body [TSSOP]



## RECOMMENDED LAND PATTERN



Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2087A





#### Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.

- 2. Package is saw singulated.
- 3. Dimensioning and tolerancing per ASME Y14.5M.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing C04-127B





Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2127A

## **APPENDIX A: REVISION HISTORY**

## **Revision D (July 2014)**

The following is a list of modifications:

- 1. Updated the title of the document.
- 2. Added the [High Gain-Bandwidth Op Amp](#page-0-0) [Portfolio](#page-0-0) table and updated all sections on page 1.

## **Revision C (June 2011)**

The following is a list of modifications:

3. Added the 2x3 TDFN (8L) package option for MCP651, SOT-23 (5L) package for MCP651S and SOT-23 (6L) package option for MCP653 and the related information throughout the document.

## **Revision B (March 2011)**

The following is a list of modifications:

- 1. Added the MCP654 and MCP659 amplifiers to the product family and the related information throughout the document.
- 2. Added the corresponding SOIC (14L), TSSOP (14L) and QFN (16L) package options and related information.

## **Revision A (April 2009)**

• Original Release of this Document.

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